

Testing S-Parameters on Pulsed Radar Power Amplifier Modules

Application Note

Products:

- R&S®ZVA8
- R&S®ZVAX24
- R&S®NRP-Z211
- R&S®BBA150
- R&S®SMF100A

This Application Note describes testing S-parameters under pulsed conditions with the R&S®ZVA vector network analyzer.

Two test setups are discussed here with regard to the source.

- Using R&S®ZVAX24 Extension unit with pulse modulator option.
- Using R&S®SMF signal generator with pulse modulator as a signal source.

In addition a constant power level calibration for applications requiring high drive power for test and measurement of device under test (DUT) is also included. A LDMOS S-band radar power transistor is used as example DUT. The pulse profile mode of the R&S®ZVA is used to analyze the time-dependent behavior of the DUT.

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1 Abstract

In many cases, devices need to be characterized using pulsed signals instead of CW signals. Stimulation of the device is provided by either a pulsed RF signal or a pulsed control voltage. One examples of this method are on-wafer measurements of power amplifiers, where heat sinks are difficult or even impossible to implement. Another example is power amplifier modules for pulsed radar systems; such modules have to deliver high peak power and cannot be driven by CW without being destroyed. This Application Note describes S-parameter measurements on a radar pulsed power amplifier module with the ZVA vector network analyzer using a new technique, pulse profile mode.

Two test setups have been described here extensively. In one test setup a SMR signal generator with pulse modulator is used as a signal source. In the second test setup, a ZVAX24 extension unit is used for pulse modulation. Other Rohde & Schwarz signal generators with a pulse-modulator option (SMR, SML, SMB, and SMA) could be used alternatively. The test setup and test procedure are described using an LDMOS S-band radar power transistor as an example. See also Application Note 1MA124 for a general overview of pulsed measurements.

The following abbreviations are used in this Application Note for Rohde & Schwarz test equipment:

- The R&S® ZVA8 Network Analyzer is referred to as the ZVA
- The R&S® ZVAX24 Extension Unit is referred to as the ZVAX24
- The R&S® NRP Z11 or higher is referred to as the Power Sensor
- The R&S® BBA 150 is referred to as the Power Amplifier
- The R&S® SMA100A signal generator is referred to as the SMA
- The R&S® SMB100A signal generator is referred to as the SMB
- The R&S® SMF100A microwave signal generator is referred to as the SMF
- The R&S® SML signal generator is referred to as the SML
- The R&S® SMR microwave signal generator is referred to as the SMR

Take extra precaution and check power rating of the inputs of all the equipments and the power at those points before connecting. This is a high power setup. Equipments such as power sensors, attenuators with insufficient power handling capabilities might be destroyed very easily. The internal couplers of the ZVA accessible via the port inputs are only designed for low powers, up to approximately 27 dBm.

2 General Description of S-Parameter Measurements with Pulse Profile Mode

To analyze the time-dependent behavior of a device during a burst, a Vector Network Analyzer (VNA) has to perform a so-called “pulse profile” measurement. Typical parameters required to characterize the time dependent behavior include rise time, overshoot, and droop. A representative pulse waveform is shown in Figure 1. For this measurement, the VNA must have time resolution significantly higher than the pulse duration. A typical VNA’s time resolution ranges from 3 to 20 μs for measurements in the frequency or time domain, which is not great enough to analyze behavior versus time with sufficient resolution. Most VNAs have a measurement bandwidth of 600 kHz or less, which is the limiting factor for high time resolution of pulse widths of 1 μs or below.

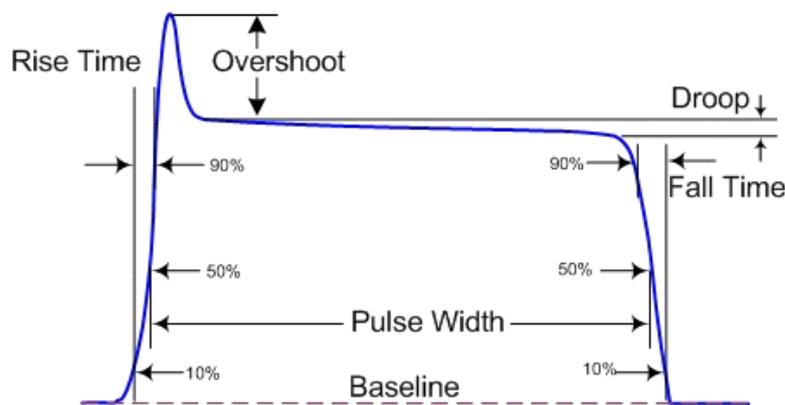


Figure 1 : A pulse waveform with various characteristics identified

To achieve resolution of better than 1 μs , additional external hardware and software can be used to “chop up” the pulsed signal into slices with different timing positions within the pulse (Figure 2). The magnitude of these pulse slices with regard to a specific delay is measured and calculated in accordance with the averaged pulse method. The delay is then increased and the next “slices” are measured until a desired portion of the pulse is analyzed. This chopping can occur in either the receiver paths at the RF frequency or directly inside the instrument in the IF path. If the IF is chopped, losses incurred by the required external switches can be minimized.

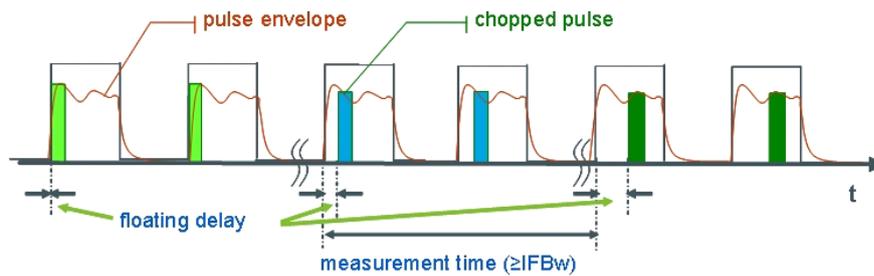


Figure 2: An example of pulse chopping

Pulse profile analysis of pulsed signals or S-parameters with pulsed stimulus is limited by the sampling rate of the A/D converter, the processing time between two data points and the available bandwidth. The sampling rate and the time required for data processing between two data points limit the time resolution, while the measurement bandwidth determines the minimum rise and fall time of the pulse that can be analyzed. A new technique developed at Rohde & Schwarz employs wideband detection and fast data recording to greatly improve pulse profile measurements.

The bandwidth-limiting factors in the analyzer are the analog bandwidth of the receivers and the capabilities of the digital signal processors (DSPs) for digital filtering. The high-end vector network analyzer R&S ZVA has an analog bandwidth of 15 MHz (with some performance degradation to 30 MHz). The IF filters of the DSPs offer adequate performance for normal CW or time sweeps with a 5 MHz bandwidth. ZVA receivers down convert the sampled data to the IF frequency at a sampling rate of 80 MHz, which results in a time resolution of 12.5 ns.

In addition to the sampling time, there is the data processing time between two measurement points, which is a bottleneck for achieving high-resolution measurements in the time domain. However, pulse profile measurement resolution can be dramatically improved by sampling the raw data and storing it directly without filtering. Instead of using hardware, the DSP software on the ZVA is used to perform digital down conversion and digital filtering after recording. The A/D converter continuously digitizes the data with a sampling rate of 80 MHz and writes it into high-speed RAM, which ensures that no delay occurs between the samples of individual measurement points, as shown in Figure 3.

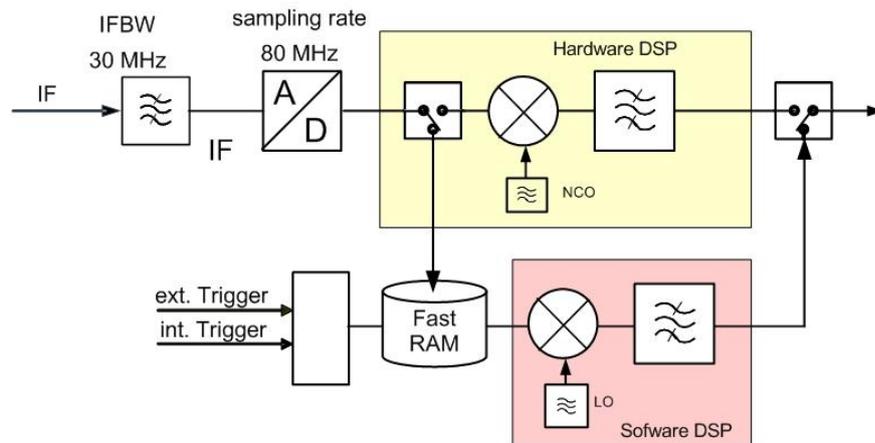


Figure 3: Fast data recording made possible with the improved high-performance pulse profile technique (option ZVA-K7 for ZVA)

Because of the high sampling rate, a measurement point is created every 12.5 ns, which is the time resolution. The trigger signal, usually derived from the rising edge of the pulse, determines the zero point in time. Consequently, the exact time relation between trigger detection and the incoming RF pulse can also be measured. This relation is especially important for determining the correct trigger delay in point-in-pulse measurements versus frequency or level.

The ZVA performs extremely-fast pulsed measurements, and with more than 10 sweeps per sec at 1001 test points, devices can easily be adjusted during the pulse profile measurement.

In addition to periodic single-pulsed signals, this new technique handles double pulses, as well as user-defined pulse trains. Devices stimulated using pulses with frequency and amplitude modulation, such as chirps, can also be analyzed.

The new techniques also benefit measurement of the S-parameters of devices with group delays in the order of the pulse width, which has been difficult or even impossible up to now. The stimulated RF signal may no longer be present at the device's input by the time the VNA receives the transmitted RF signal from the output. A correct S₂₁ parameter can only be measured with temporal signal overlapping. Using the new technique, the VNA solves this problem by applying a time offset to the wave quantities. Before calculating the S-parameters, it mathematically shifts the wave quantities by the device's group delay. A specific time delay can be assigned to each wave quantity depending on the measurement direction, so the VNA correctly displays the gain (S₂₁) versus the entire pulse duration.

3 Point in Pulse Measurement

The point-in-pulse measurement enables accurate S-parameter and power measurements to be made, allows the moment of data acquisition within the pulse to be easily shifted, and eliminates the dependency of dynamic range on duty cycle. However, it requires a VNA with a wide measurement bandwidth. Using the point-in-pulse measurement technique, the pulse is monitored only during the “on” phase of the RF bursts so the sampling time (T_{spl}) to acquire the raw data of a wave quantity or an S-parameter must be shorter than the pulse width, t_{on} (Figure 4).

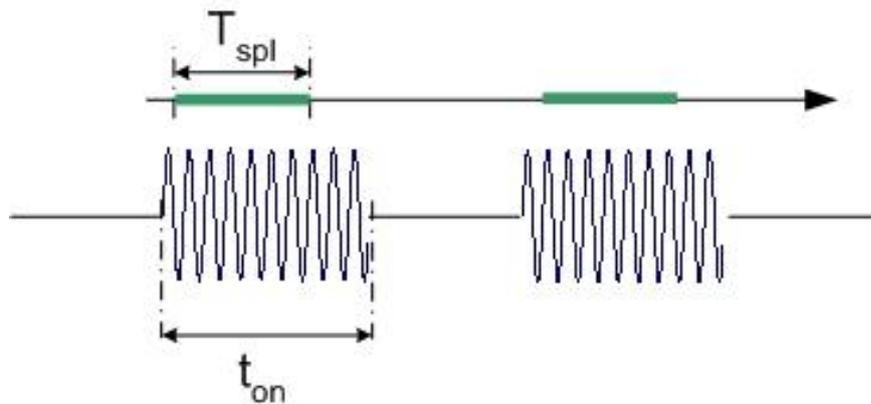


Figure 4: Sampling time for point-in-pulse measurements

The sampling time is determined mainly by the receiver’s measurement bandwidth, and minimum sampling time and measurement bandwidth is defined as $T_{spl} \approx 1/IFBW$. This means that with increasing measurement bandwidth, sampling time decreases and shorter pulses can be analyzed. VNAs implement IF filters digitally and typically offer measurement bandwidths up to 600 kHz, so the sampling time is 1 μ s or more. Some network analyzers, such as the R&S ZVx Series, have IF bandwidths of 5 MHz or more, which allows sampling times as fast as 400 ns with a 5 MHz bandwidth. The sampling process should only occur during the on-phase of the pulse, so a trigger signal synchronous to the RF pulse is necessary to synchronize the data acquisition of the VNA with the on-period of the pulse. The VNA is used in “point-trigger mode”, which means that data sampling for every measurement point starts after the detection of a trigger event.

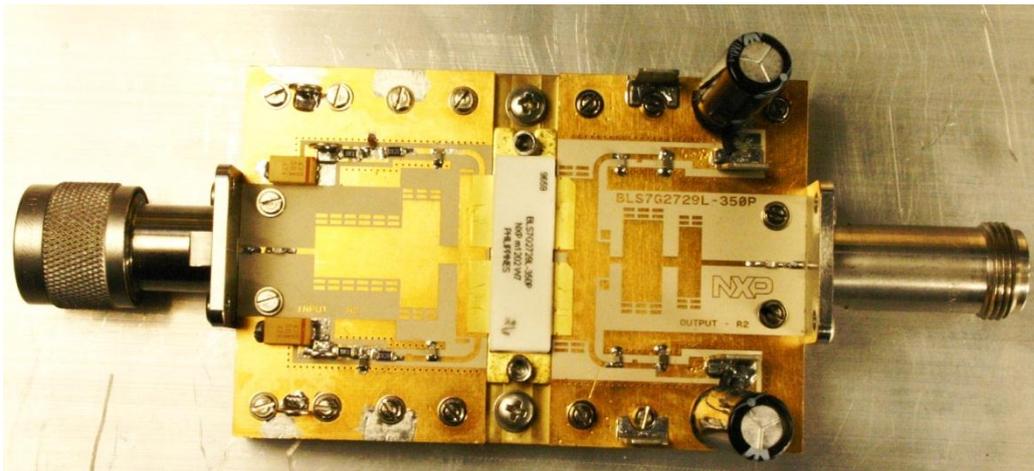
Active devices such as amplifiers often show settling or ringing effects at the beginning of the pulse, but designers are typically interested in device behavior after it has settled. By selecting a suitable trigger delay, the start of the sampling process can be shifted to the quiet pulse roof of the amplifier. Dynamic range and sensitivity using the point-in-pulse method depends on sensitivity and the measurement bandwidth of the receivers, which are independent of the duty cycle of the RF pulse. Consequently, dynamic range depends on pulse width, which determines sampling time and thus the required measurement bandwidth. Averaging can be applied to increase dynamic range by maintaining the measurement bandwidth. Ten times averaging in the IQ domain (for example) increases the dynamic range by a factor of 10.

4 High-Power Transistor Test Setup

The DUT used in our application note is an S - Band LDMOS Pulsed Radar Power Transistor in an RF test fixture with N connector.

Condensed data of the NXP BLS7G279L - 350P LDMOS S-Band pulsed radar power transistor		
Frequency range	2.7 GHz to 2.9 GHz	
Output Power	350 W	At a duty cycle of 10% and 300 μ s pulse width.
Gain	13.5 dB	

Table 1: Condensed data of the DUT (NXP BLS7G279L - 350P LDMOS S-Band Pulsed Radar Power Transistor)



Device Under Testing NXP BLS7G279L - 350P LDMOS S-Band Pulsed Radar Power Transistor

4.1 Test Setup using SMF (Signal Generator)

The internal couplers of the ZVA accessible via the port inputs are only designed for low powers up to approximately 27 dBm. Figure 5 shows the test setup in detail. The pulsed output signal of the SMF is amplified to the required drive power by a power amplifier operating in linear mode. Part of the input power and of the reflected power of the amplifier module under test (DUT) is coupled by a bidirectional coupler and reduced by attenuators (20 dB) to the levels suitable for the ZVA reference and test inputs. The DUT output is connected to a 30 dB power attenuator. A part of the attenuated output signal is coupled by the directional coupler and fed via another 10 dB attenuator to port 2 of the ZVA.

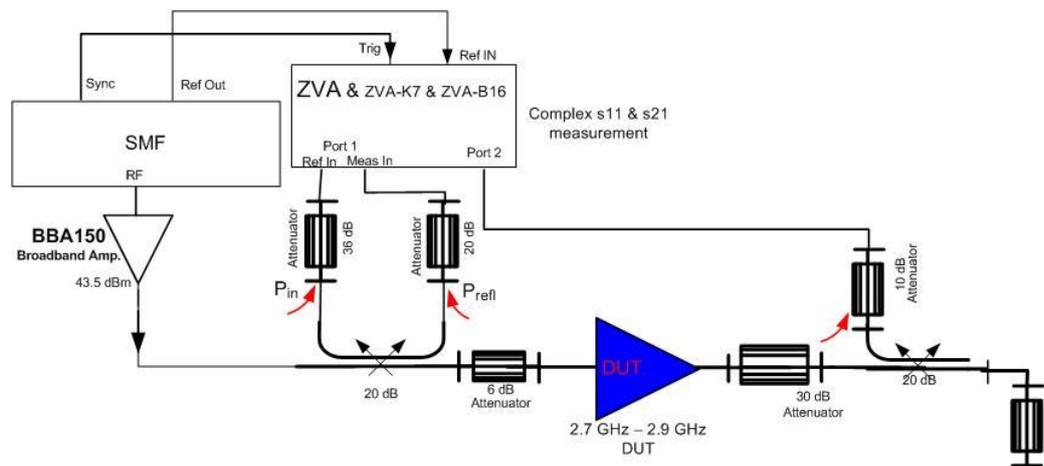


Figure 5: Test setup for characterizing radar pulsed power transistor with the ZVA and SMF

The Sync output of the SMF triggers the ZVA for pulse-synchronous analysis. The SMF also provides a 10 MHz reference signal for the ZVA in order to eliminate frequency deviations between the SMF transmit signal and the ZVA receive signals. The ZVA must therefore be set to external reference.

In the case of unavailability of an SMF signal generator, the same test setup is possible using the ZVAX24 Extension Unit. In this Application note, we discuss in detail the test setups and the test results obtained using the ZVAX24 Extension unit.

4.2 Test Setup using ZVAX24 (Extension Unit)

Due to the high drive power required (approx. 22 W) and the considerably higher output power (approx. 350 W), a test setup with external couplers is necessary. The internal couplers of the ZVA accessible via the port inputs are only designed for lower powers up to approximately 27dBm.

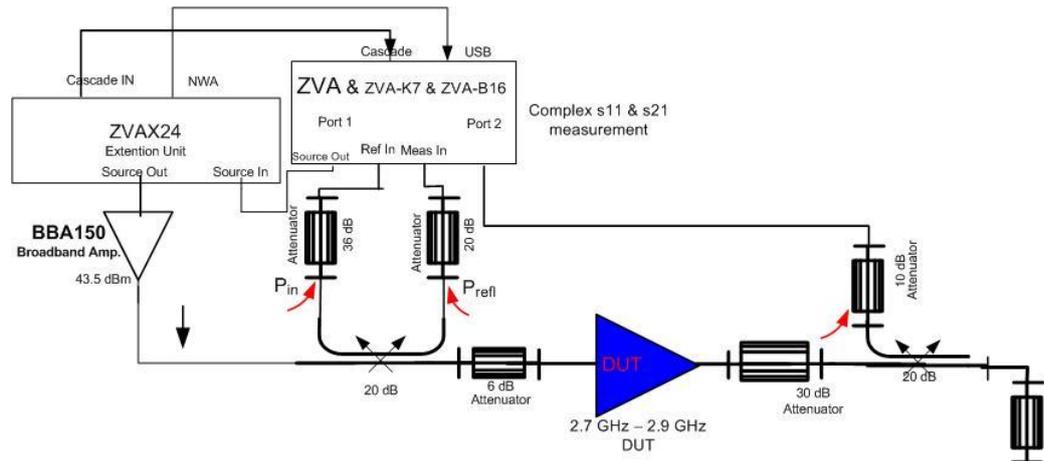


Figure 6: Test setup for characterizing radar pulsed power transistor with the ZVA and ZVAX24

Figure 6 shows the test set up in detail. The pulsed output signal from the extension unit is amplified to the required drive power by a power amplifier operating in the linear mode. Part of the input power and of the reflected power of the amplifier module under test (DUT) is coupled by a bidirectional coupler and reduced by attenuators (36 dB) to the levels suitable for the ZVA reference and test inputs. The DUT output is connected to a 30 dB power attenuator. A part of the attenuated output signal is coupled by the directional coupler and fed via another 10 dB attenuator to port 2 of the ZVA.

5 Pulse Profile Measurement

5.1 Measurement Principle

The pulse modulator option R&S ZVAX24 provides a pulsed source signal at the VNA port 1. Pulse width and period are determined by the internal pulse generator of the VNA provided by option R&S ZVAB27. This option also provides a second “Sync” signal that can be used to synchronize the measurement to the rising edge of a generated pulse.

The DUT is connected between the test port 1 and test port 2 of the analyzer. The transmitted pulsed signal is measured at port 2 using the analyzer’s “Pulse Profile” mode.

The measurement involves the following steps,

1. Connect the ZVAX24 extension unit.
2. Configure the extension unit for the selected measurement and test setup (“ZVAX Path Configuration”).
3. Define of the pulse generator and the trigger setting.
4. Configure of the “Pulse Profile” mode.
5. Calibrate (Power calibration and system error calibration).
6. Connect the DUT and perform the measurement.

Power calibration and system error correction for test setups with the extension unit can be performed in the ordinary way. However, care must be taken while connecting the power sensor.

The input power rating of every device must be taken in account since this is a high power measurement setup.

5.2 Connecting the ZVAX24 Extension Unit

The pulse profile measurement requires the following connection between the network analyzer and the extension unit.

- RF connection: Connect SOURCE IN (ZVAX) to SOURCE OUT (ZVA) and SOURCE OUT (ZVAX) to RF-IN (BBA150).
- Control Connection: Connect USB from NWA (ZVAX) to any of the USB type A connectors at the front and rear panel of the ZVA.
- Pulse Generator Connection: Connect CASCADE IN (ZVAX) to CASCADE (ZVA) using the RJ - 45 cable supplied with the extension unit.

5.3 ZVAX Path Configuration

After the extension unit is connected to the network analyzer as described in the previous section, it is possible to select the modules to be looped into the signal path(s) and the routing of the pulse generator signals. This is done in the “ZVAX Path Configuration” dialog (“Channel>Mode>ZVAX Path Configuration”). The schematic in this dialog shows all RF modules that are installed in the extension unit.

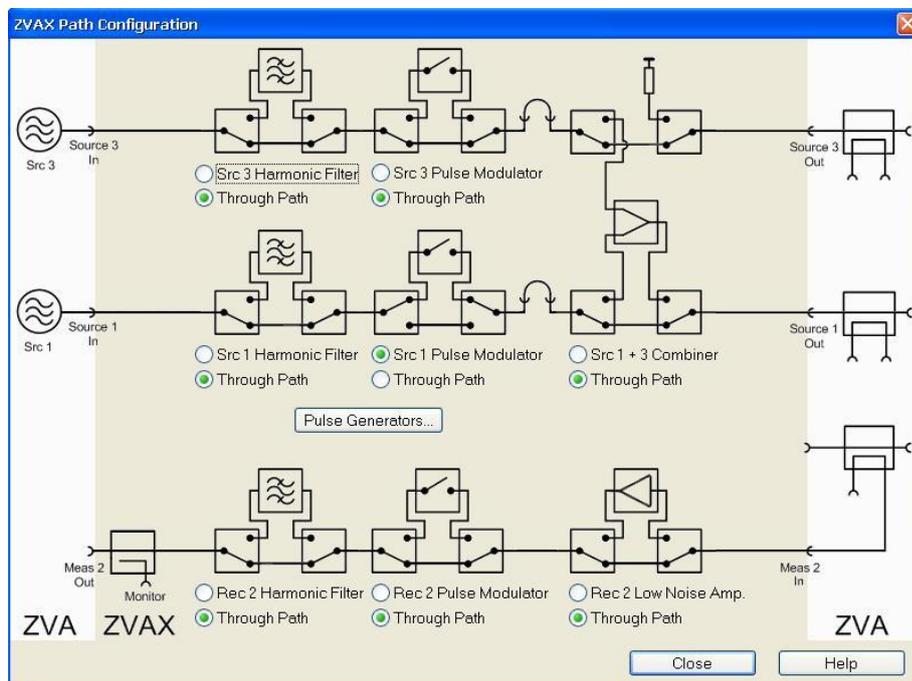


Figure 7: ZVAX Path Configuration

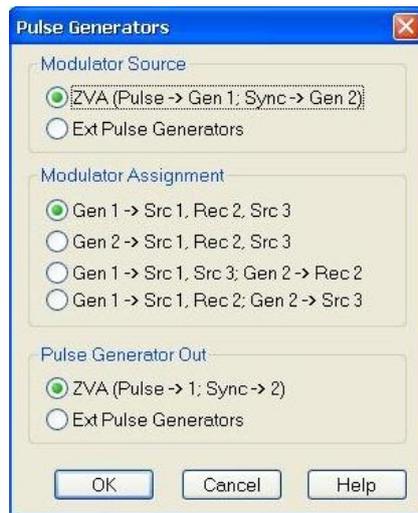


Figure 8: ZVAX Path Configuration (Pulse Generator)

- a) Use the radio buttons in the “ZVAX Path Configuration” dialog to activate the “Source 1 Pulse Modulator”. If your extension unit contains a harmonic filter or combiner, select the corresponding Through paths (Figure 7).
- b) Press “Pulse Generators” and make sure that the “Modulator Source” and the “Modulator Assignment” settings are as shown in Figure 8.

5.4 Setting up the pulse profile mode of the ZVA

The dialog box for setup of ZVA pulse profile mode parameters are shown in Figure 9.

Start and stop time parameters are set to $-3\ \mu\text{s}$ and $35\ \mu\text{s}$ (recording length is thus $38\ \mu\text{s}$) to center the pulse with in the display. The bandwidth is set to 10 MHz for fast time response. Source power is set to $-60.7\ \text{dBm}$. But this is automatically set when we input the channel base power as $-60.7\ \text{dBm}$. The center frequency is set to 2.8 GHz since the working range of the DUT is specified between 2.7 GHz – 2.9 GHz.

1. Click "Channel > Sweep > Sweep Type > Pulse Profile" to activate the pulse profile mode.
2. Click "Define Pulse Profile" and configure the "Time Parameters" as stated

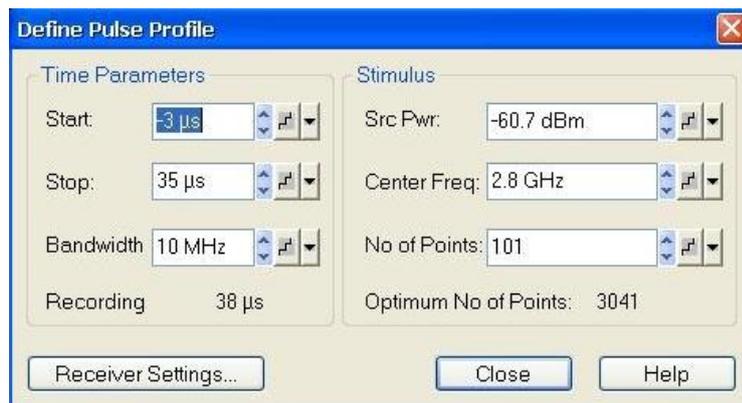


Figure 9: Pulse profile parameter setting

Number of points can be selected as desired.

Define Pulse Profile adjustment is done to define what is seen of the screen of the ZVA. The time parameters can be altered to zoom into certain parts the pulse. For example, the start and stop time can be adjusted to $-3\ \mu\text{s}$ to $8\ \mu\text{s}$ for displaying just the beginning of the pulse.

5.5 Pulse generator signals

The pulse generator provides single pulses with defined width and period or sequences of pulses (pulse trains). For our test setup we use the option “Single Pulse”. A single pulse with a width of $30\ \mu\text{s}$ is generated. The pulse is repeated after a pulse period of $300\ \mu\text{s}$.

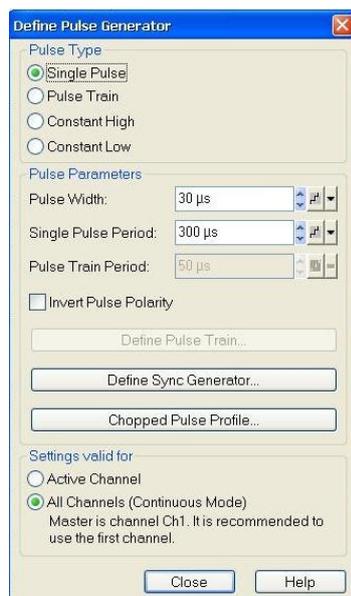


Figure 10: Pulse profile parameter setting

Define Pulse Generator adjustment defines the parameter of the pulse that is generated.

1. Click "Channel > Sweep > Sweep Type > Pulse Generator" to activate the pulse generator signal.
2. Click "Def Pulse Generator" and configure the "Pulse Parameters" as shown above.
3. In the "Define Pulse Generator" dialog, click "Define Sync Generator..." and ensure that the "Sync" signal is configured as shown below.
4. Click "Channel > Sweep > Trigger > Pulse Gen..." to select the pulse generator as trigger source. The dialog "Pulse Gen Trigger" opens. Close it without modifying the default setting ("Rising Edge Sync").

5.6 Setting up the pulse modulation of the SMF

Setup the pulse modulation parameters for the SMF as shown in Figure 11. Pulse period and pulse width are in accordance with the specifications of the power amplifier module under test.

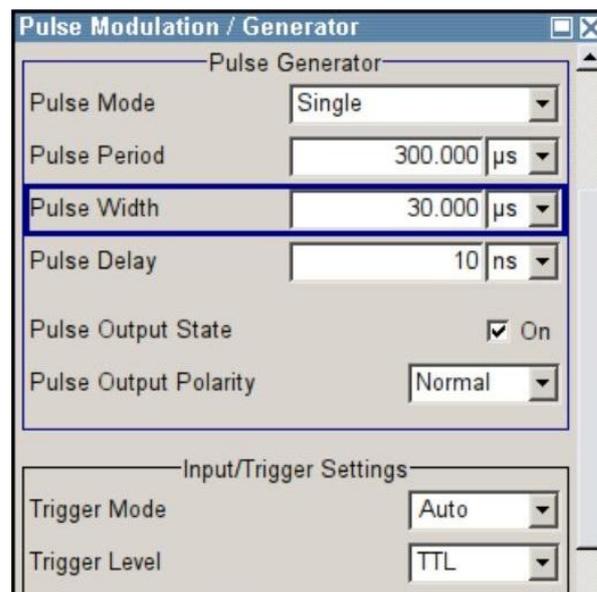


Figure 11: Pulse modulation parameter setting of the SMF

6 Calibration

Calibration is one the major steps in any test and measurement setup. The requirement of the constant power level is fulfilled by the proper power calibration on source and receiver test port. And for the compensation of system related errors, the calibration for system error correction is a must. Figure 12 and Figure 13 shows the test setups for testing and measurement purpose of high drive power requirement applications.

6.1 One Path Two-Port Calibration of Test Setup

The calibration of the ZVA is performed in the pulse profile mode. The module under testing is removed and the two associated ports are the calibration plane.

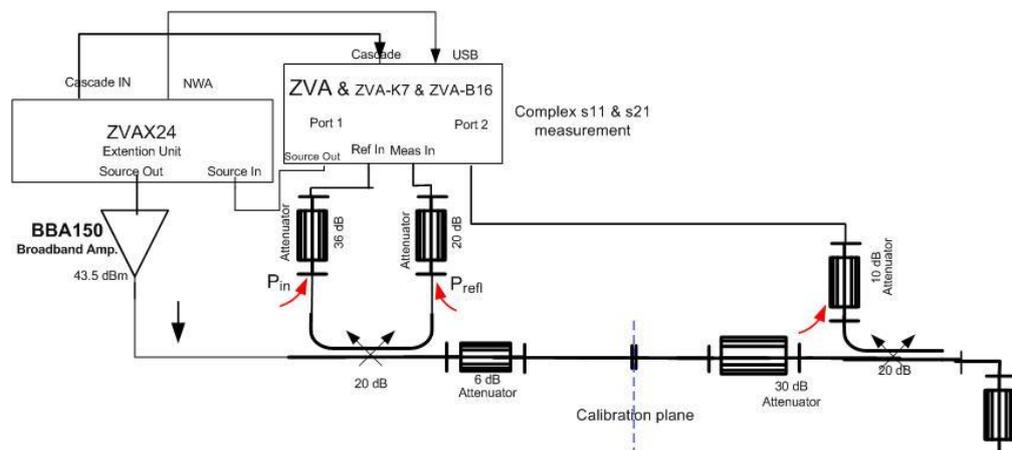


Figure 12: Calibration Setup for Characterizing a Radar Pulsed Power Transistor with the ZVAX24

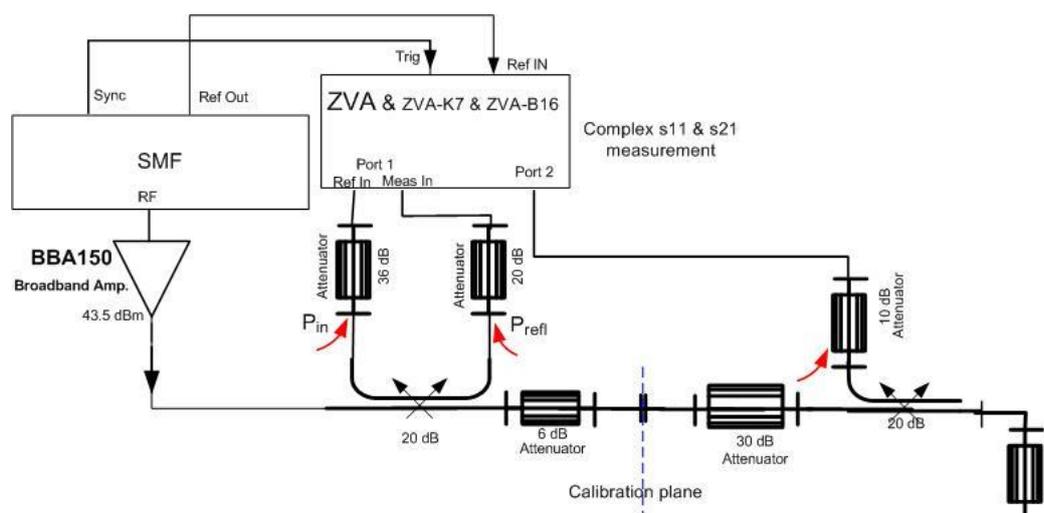


Figure 13: Calibration Setup for Characterizing a Radar Pulsed Power Transistor with the SMF

Due to the needed high pulse power of the device under test and the corresponding high attenuation between the amplifier's output and port 2 of the network analyzer, noise during the calibration of S21 is increased and then superimposed on the subsequent measurement. This effect can be considerably reduced by decreasing the measurement bandwidth to 100 KHz for calibration.

For measurement on the DUT, restore the original 10 MHz measurement bandwidth. Three types of calibration were performed in total. First the source power calibration is performed to achieve constant linear power at the source test port. The receiver power calibration is performed next. This is done to make the source and the receiver resemble each other. And finally the one path two-port calibration is performed as a system error correction procedure.

A detailed description on how to perform each individual calibration is provided later in this application note.

The following measurements are obtained using a through connection between the test ports at the calibration plane.

Figure 14 shows the magnitude plot of the incident wave at port 1 (a1) and the magnitude of reflected wave of port 2 (b2). Both the traces are in the dBm scale. The markers M1, M2 and M3 are placed at 2.1 μ s, 8.2 μ s and 29.06 μ s. Coupled markers are used here. The time scale used can be defined in the dialog "Define Pulse Profile". To do that, the sweep type Pulse Profile must be activated first. The pulse period for this particular DUT is 300 μ s at 10% duty cycle. So the pulse width is set as 30 μ s from the pulse generator.



Figure 14: Single Path Two port calibration of test setup. The magnitude plot for a1 and b1 for the entire pulse duration.

Figure 15 shows the magnitude plot of input complex reflection coefficient (S11) and the forward complex transmission coefficient (S21). The green trace is S11 and the red trace is S21.

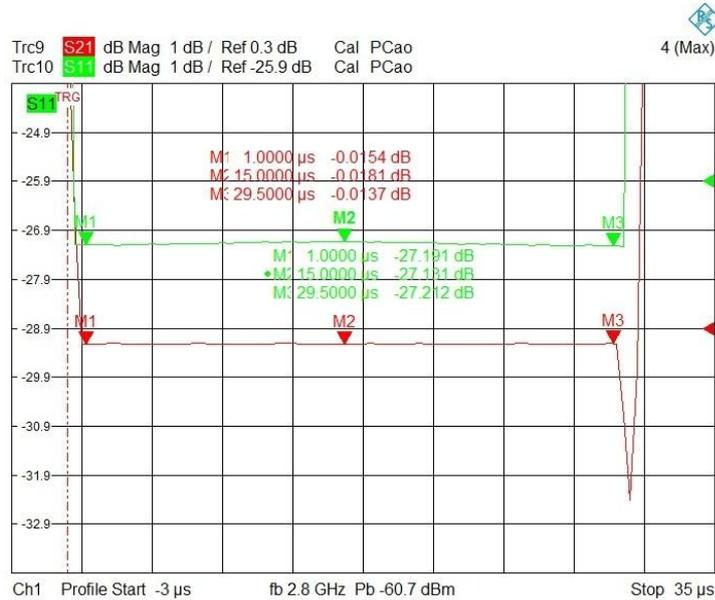


Figure 15: Single Path Two port calibration of test setup. The magnitude of S11 and S21 for the total pulse width.

Figure 16 shows the magnitude and the behavior of the phase plot of S21 during the total pulse width of 30 μs.

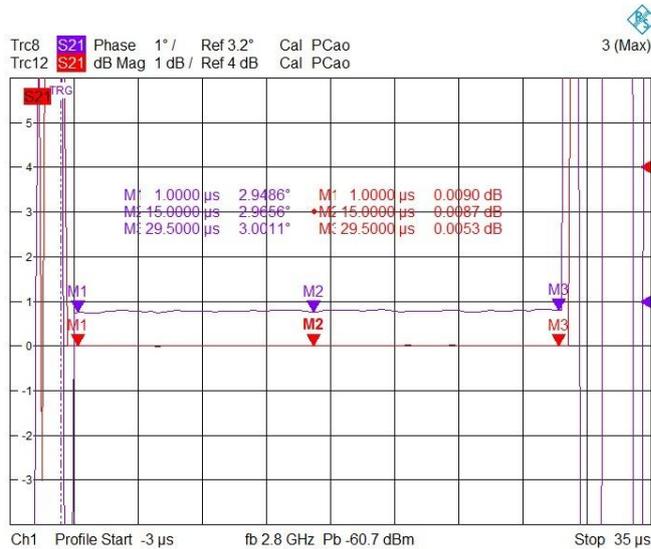


Figure 16: Single Path Two port calibration of test setup. The magnitude and phase plots of S21 for the total pulse width.

Figure 17 is a collaborative plot of the previous plots in one screen for easy comparison of measurement data.

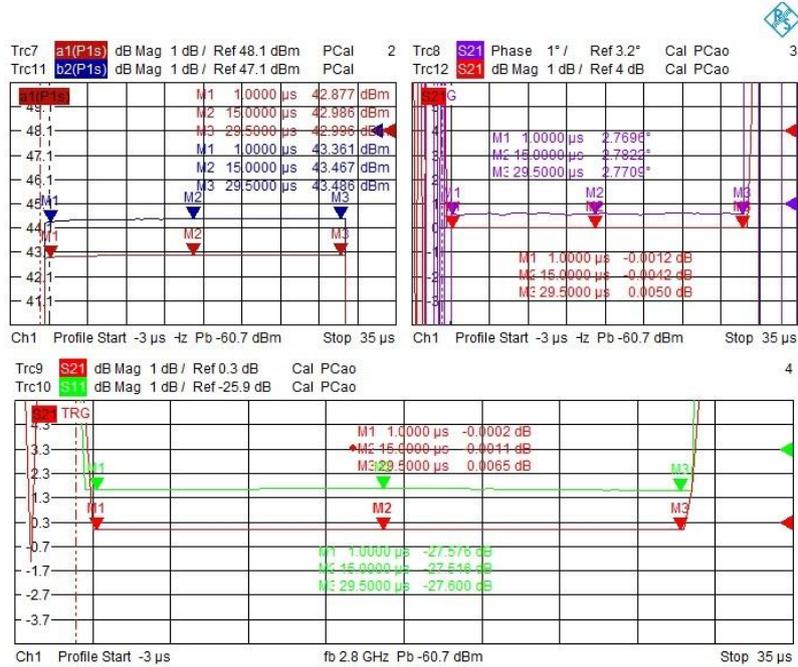


Figure 17: Single Path Two port calibration of test setup. The noise of S21 can be reduced by reducing the measurement bandwidth to 100 KHz during calibration.

Figure 18 shows in detail the magnitude plot of S11 and incident and reflected waves a1 and b1.

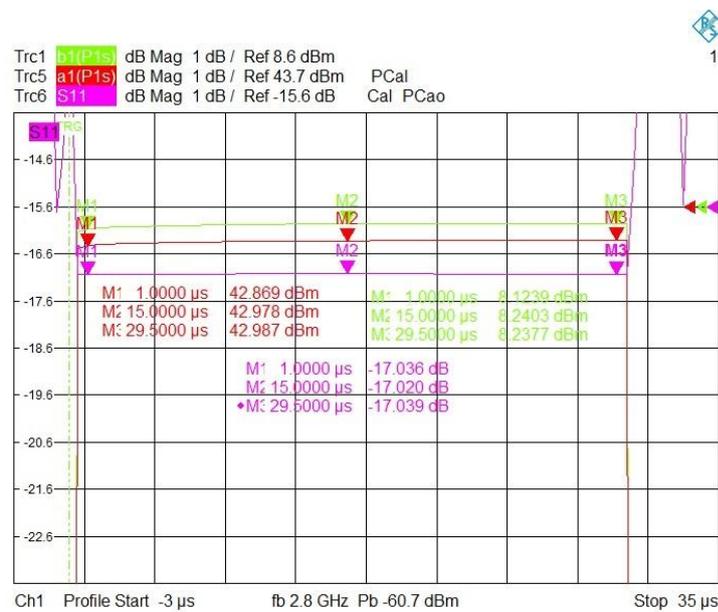


Figure 18: Single Path Two port calibration of test setup. The magnitude S11, the wave quantity a1 and b1 for the total pulse width.

6.2 Power calibration

Since this is a high power setup, linearity in the output of the driver amplifier is required. The power calibration in this case becomes highly important and forms a very significant part of the entire test and measurement procedure. After all connections are made as shown in the test setup (Figure 12 or Figure 13), the calibration is carried out at the calibration plane.



Power Sensor with 30dB Attenuator (used for power sensor protection)

A 30 dB input attenuator is placed in front of the power sensor and the input source test port. The input power rating of the attenuator for our case is 100W. For the purpose of our DUT testing we require up to maximum 30 W (44dBm) input power. The purpose of attenuator is to protect our power sensor. We are using a Rohde & Schwarz NRP-Z211 two-path diode sensor (-60 dBm to +20dBm).

For this application note a BBA150-D60 Broadband Amplifier was used. The BBA150-D30 can also be used even though not recommended. The BBA150-D30 has its 1dB compression point at 38W in the 2.7GHz to 2.9GHz frequency range and hence may involve a small compromise in drive signal linearity. We will calibrate so that at the input of the DUT there is a constant power of 43.3 dBm for the frequency span of 2.5GHz to 3GHz. The DUT's operating frequency range is 2.7 GHz to 2.9 GHz.

6.2.1 Source Power Calibration

Step 1 ZVA configuration for Power Calibration (Switch off power amplifier)

Connect the power sensor to the USB of the ZVA.

Setting power limit

System > System Config. > Power

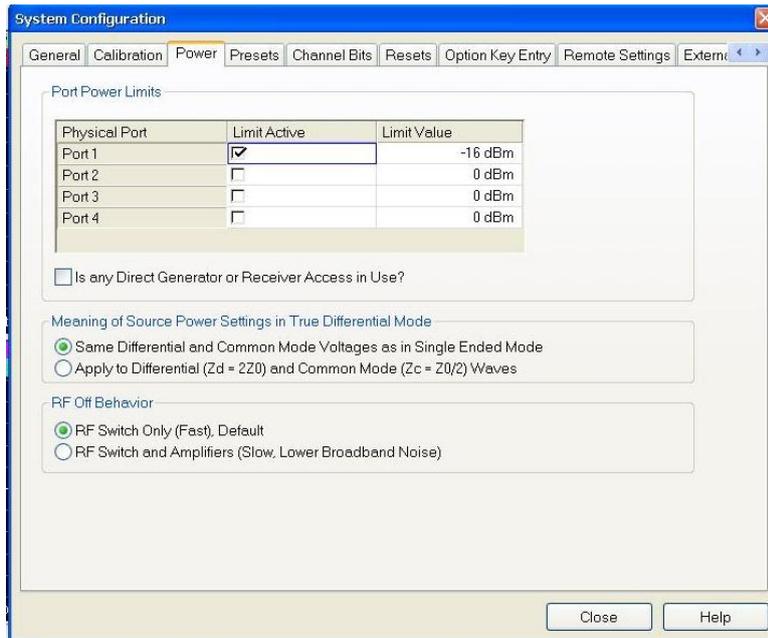


Figure 19: Calibration settings

Channel base power setting:

Channel > Power Bandwidth Average > Power > -60.7 dBm

Step Attenuator Setup

Channel > Power Bandwidth Average > Step Attenuator >

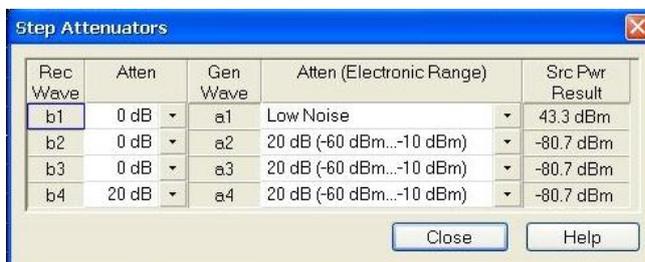


Figure 20: Calibration settings

Measurement Bandwidth Selection (Lower noise of S21)

Channel > Power Bandwidth Average > Meas Bandwidth > 100KHz

Number of points (For faster calibration)

Channel > Sweep > No of points > 11 or 21

It is recommended to perform option 1 and then again option 2 if tests on the DUT are carried out in Pulse Profile Mode.

Sweep type

Option 1 (Linear Sweep)

Channel > Sweep > Sweep Type > Lin Frequency

Start Freq: 2.5 GHz

Stop Freq: 3 GHz

Pulse Generator Activation

Channel > Mode > Pulse Generator

Pulse Gen. Setup

Channel > Mode > Def Pulse Generator

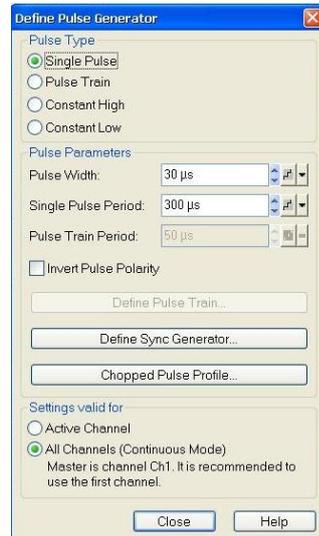


Figure 21: Calibration settings

Option 2 (Pulse profile)

Channel > Sweep > Sweep Type > Pulse Profile

Channel > Sweep > Sweep Type > Define Pulse Profile

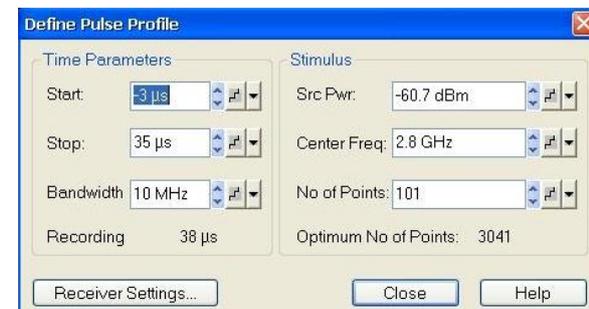


Figure 22: Calibration settings

Pulse Generator Activation

Channel > Mode > Pulse Generator

Pulse Gen. Setup

Channel > Mode > Def Pulse Generator

The pulse train with Pulse Train Period 300µs can also be selected.

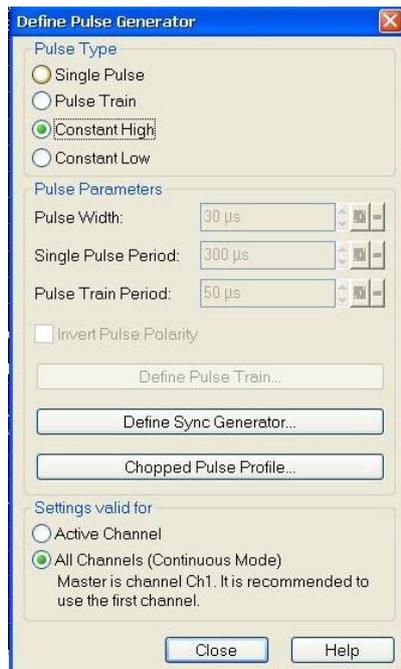


Figure 23: Calibration settings

Common for both Option 1 and Option 2

Trigger Settings

Channel >Sweep >Trigger > Pulse Gen



Figure 24: Calibration settings

External Power Meter Configuration

System > System Config> External Power Meters (automatic detection and config.)

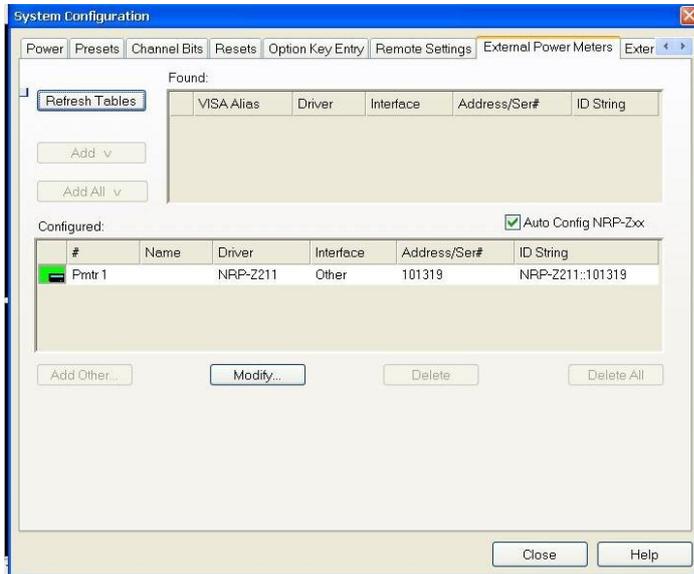


Figure 25: Calibration settings

Power Calibration

Channel > Calibration > Power Corr All Ports On (Tick sign appears after activation)

Source Power Calibration

Channel > Calibration > Start Power Cal > Source Power Cal

Modify Source Power Cal. Setting

Click Modify settings

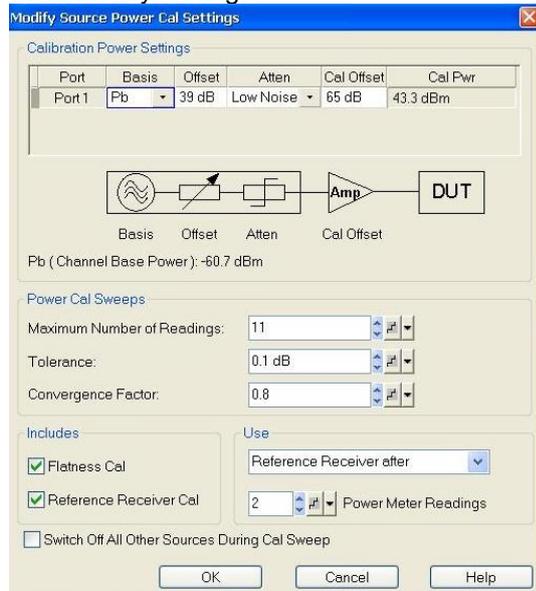


Figure 26: Calibration settings

For this step we have to manually insert the value of Offset and Cal Offset. Click on the drop down box for Atten and select Low Noise Amplifier. The Cal Offset is set to a value higher than the gain of the amplifier and the offset value is adjusted so that the Cal Pwr is 43.3 dBm.

For hand calculation:

$$Pb + \text{Offset} + \text{Cal Offset} = \text{Cal Pwr} \quad (-60.7+39+65=43.3 \text{ dBm})$$

Pb = Channel base power (it is set automatically from previous steps)

For higher accuracy in the power calibration process we recommend using:

Maximum Number of reading: any value greater than 5.

Tolerance: 0.1 dB

Convergence Factor is set to a value less than 1.

Recommended settings:

Select both Flatness Cal and Reference Receiver Cal. Also select Use Reference Receiver After. And select a value greater than 1 for power meter reading.

Figure 26 shows the setting used in this application note for test and measurement on our DUT. For your application we suggest you tryout other values and select a suitable setting for your application.

Power Meter Correction

Add Point > 2.5 GHz > -36 dB Transmission Coef.
 Add Point > 3 GHz > -36 db Transmission Coef. > OK

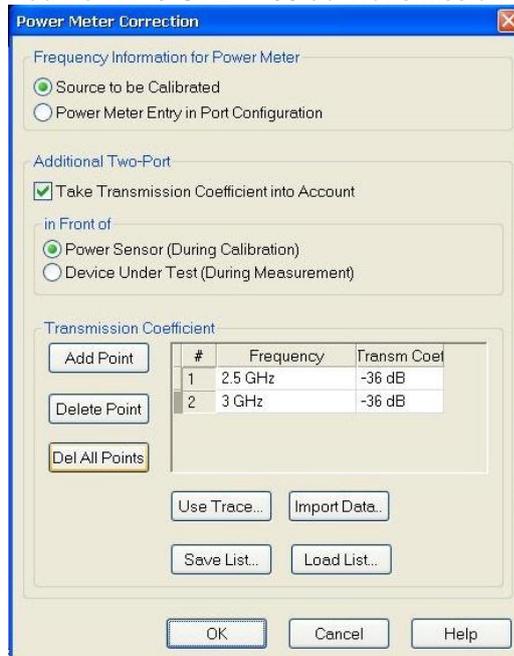
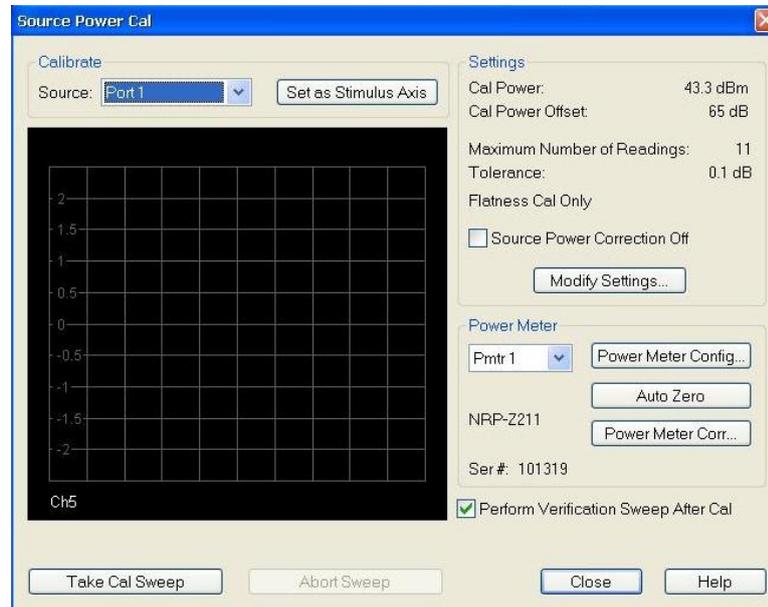


Figure 27: Calibration settings

Switch on power Amplifier (allow for warm up time)**Figure 28: Calibration settings**

Click Take Cal Sweep

For ideal source power calibration we can expect a constant flat line at 43.3 dBm with little swing (typically 0.2 dB).

6.2.2 Receiver power calibration

Make a through connection between the Source Test Port and the Output Test Port at Calibration Plane

Channel > Calibration > Start Power Cal > Receiver Power Cal

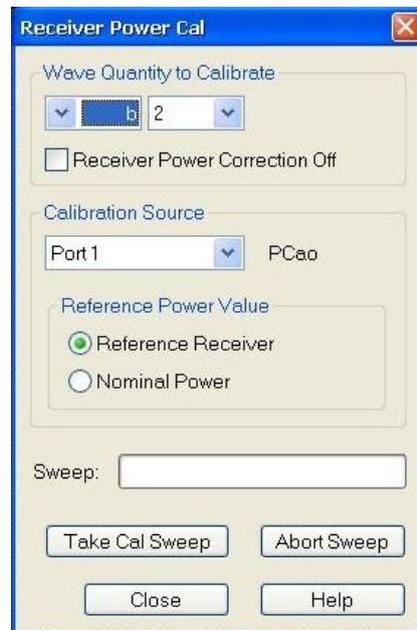


Figure 29: Calibration settings

Click Take Cal Sweep

Remove the Power Sensor and Input Attenuator (30 dB) from the test port.

6.2.3 Calibration for System Error Correction

Channel > Calibration > Start Cal > Two Port P1-P2 > One Path Two-port

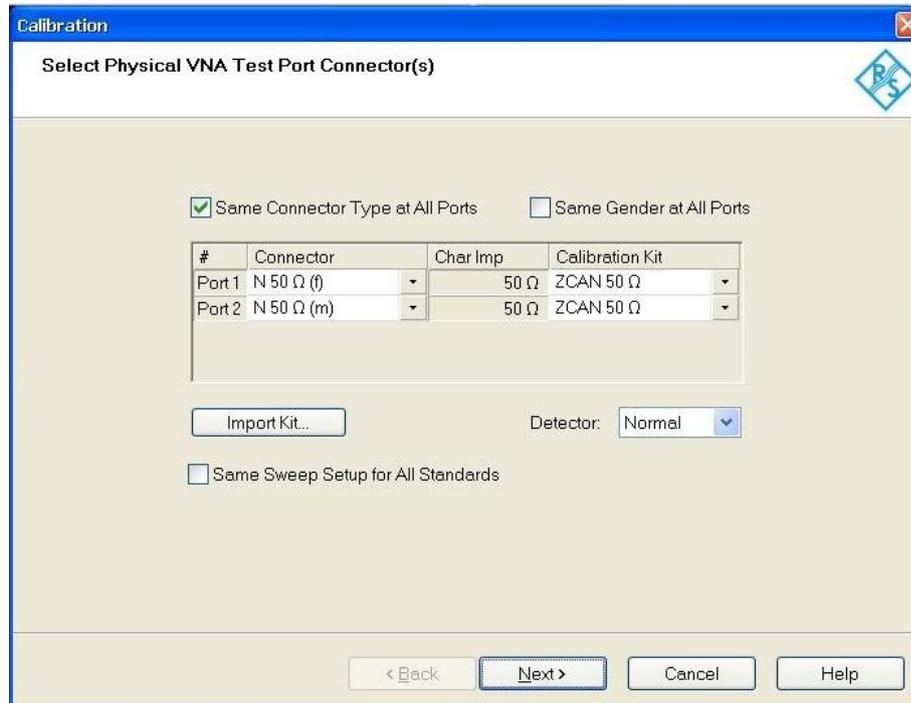


Figure 30: Calibration settings

Click Next.

Perform the normal calibration procedure. For our purpose we are using N-port ZCAN calibration Standard.

Open, Short, Match and Through.

The entire calibration process is now complete. Now connect the test ports to the DUT. And the setup up is ready for test and measurements.
(Figure 5 or Figure 6)

7 Test Results

The following test results are derived from the pulsed profile measurements carried out on an LDMOS S-band radar power transistor (BLS7G2729L- 350P) as DUT. The frequency on interest is within the range of 2.7GHz and 2.9GHz. The center frequency is to 2.8 GHz. The measurement bandwidth is set to Fine Adjust. The pulse profile mode is activated. The pulses are of 300µs period at 10% duty cycle. Pulse width is thus set to 30 µs.

Figure 31 shows the combined general plot of the DUT test setup under Pulse Profile measurement. There are 4 diagram areas on the same channel. To add a new diagram area Trace > Trace Select > Add Trace + Diag Area

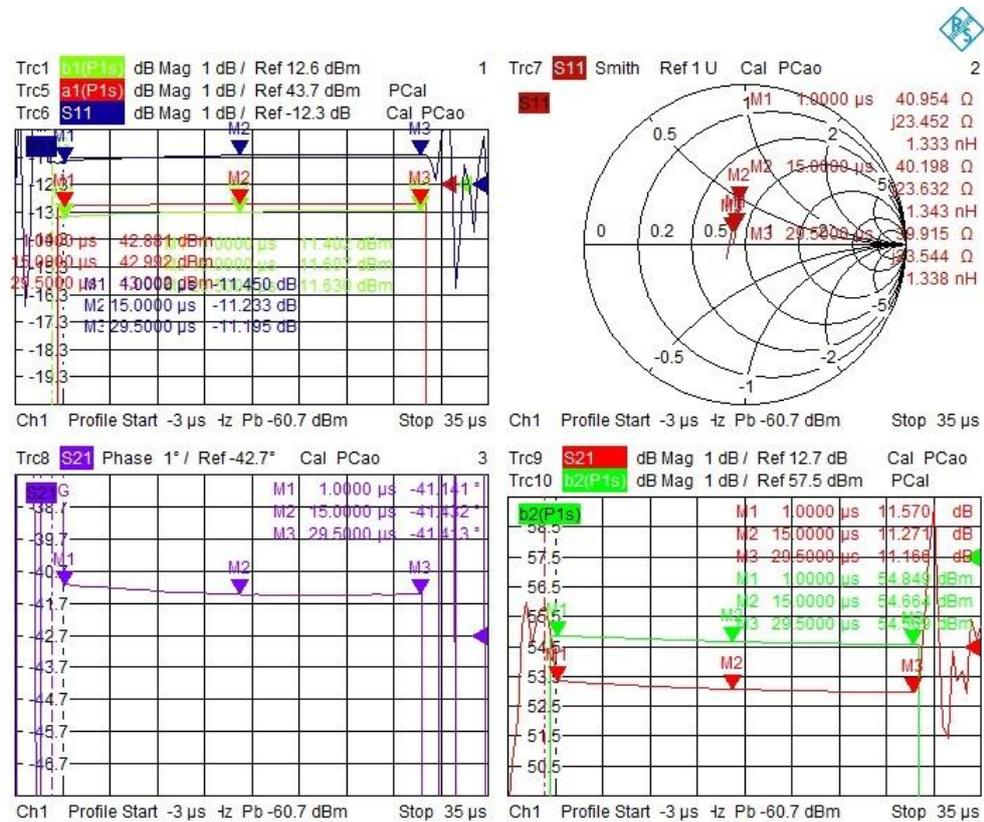


Figure 31: Test results of the pulse profile measurement (general)

Figure 32 shows the behavior of the S11 parameter using Smith Chart output. To activate the Smith Chart plot, *Trace > Format > Smith*.

To get a detailed view of one diagram area (Figure 32) instead of a combined general screen view of all the diagram areas (Figure 31), double click anywhere on the diagram area of interest. Next, using the toolbar click on *Trace > Measure > S11*. The front panel can also be used instead.

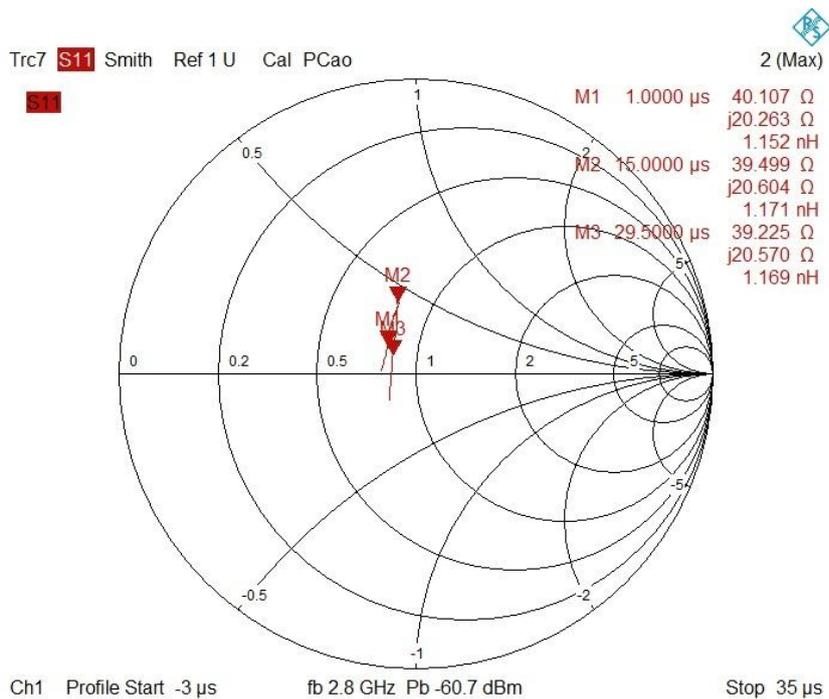


Figure 32: Test results of the pulse profile measurement. The smith chart plot of S11.

Figure 33 shows the magnitude of S11, b1 and a1 for the total duration of the pulse width.

Markers data can be moved from the top right to any place on the screen. Right click on the marker data and select moveable marker data. Now reposition at your own convenience.

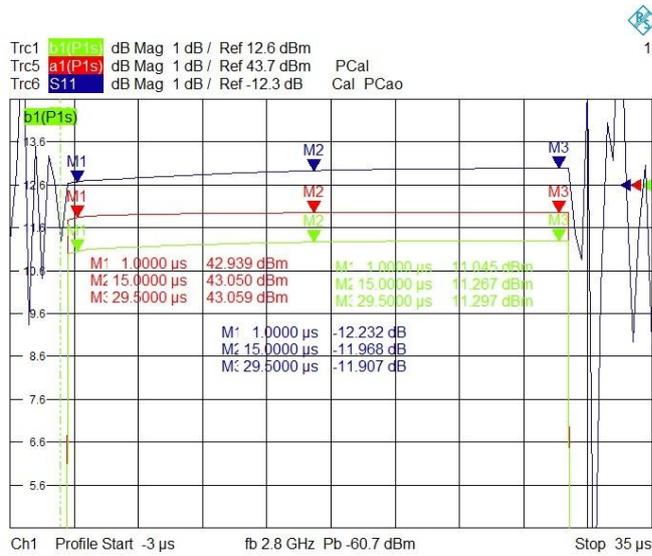


Figure 33: Test results of the pulse profile measurement. The magnitude of S11, magnitude of wave quantities b1 and a1 for total pulse width.

Figure 34 shows the magnitude plot for incident wave quantities a1 and b2 for source at port 1 of ZVA.

For the measurement of wave quantities, click *Trace>Measurement>Wave Quantities > a1*. For adding a second trace in the same diagram area *Trace> Add Trace*. Next, *Trace>Measurement>Wave Quantities > b1*

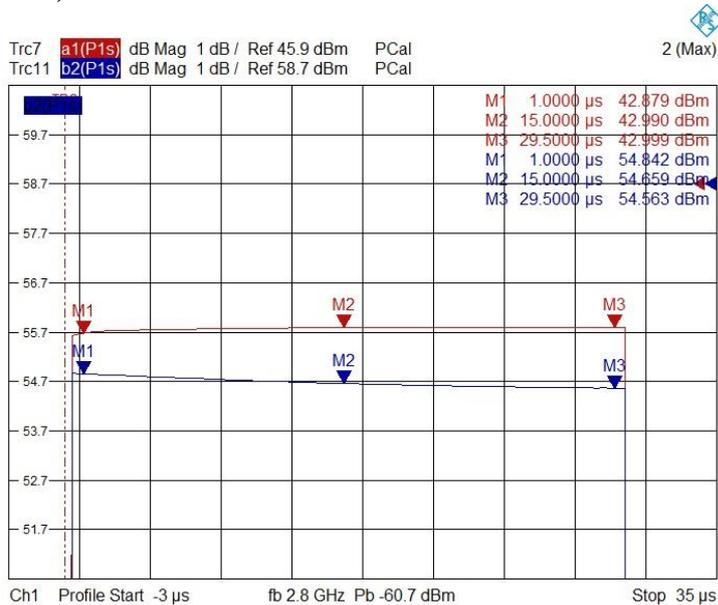


Figure 34: Test results of the pulse profile measurement. The magnitude of a1, magnitude of b2 for total pulse width.

Figure 35 shows the gain and output power measurement for the total duration of the pulse width. For changing the scaling in the dB axis for individual traces *Trace>Scale>Scale / Div*. In Figure 35 we selected Scale per division of 1 dB in order to increase precision and sensitivity of the measurements.

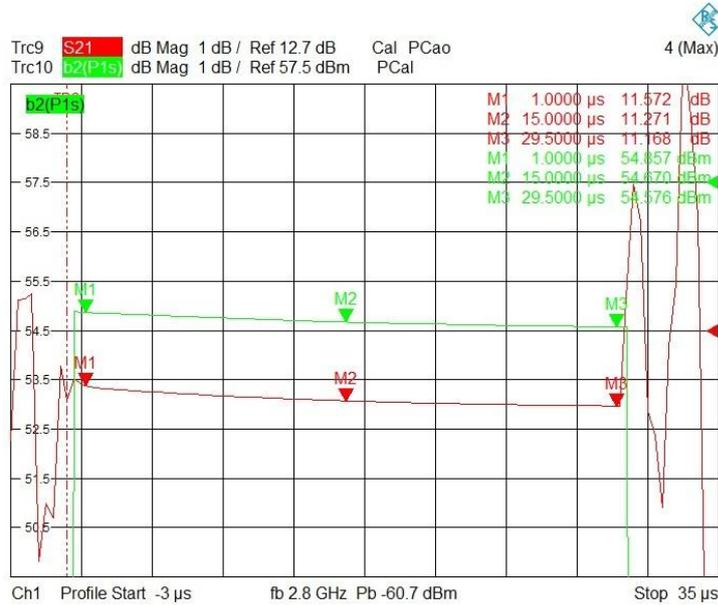


Figure 35: Test results of the pulse profile measurement. The magnitude of S21, magnitude of b2 for total pulse width.

Figure 36 shows the Gain and Output Power measurements results over the operating frequency range.

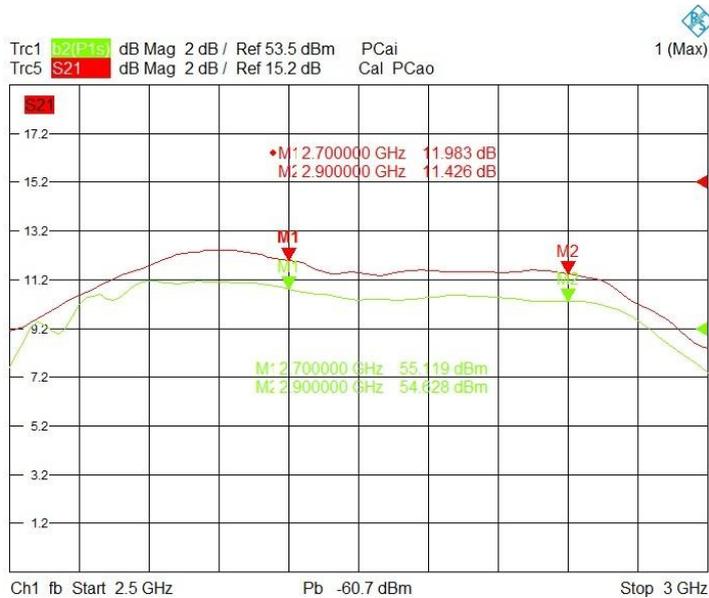


Figure 36: Test results of the pulse profile measurement over the operating frequency range.

Figure 37 shows the behavior of the phase of S21 over the total pulse width of 30µs.

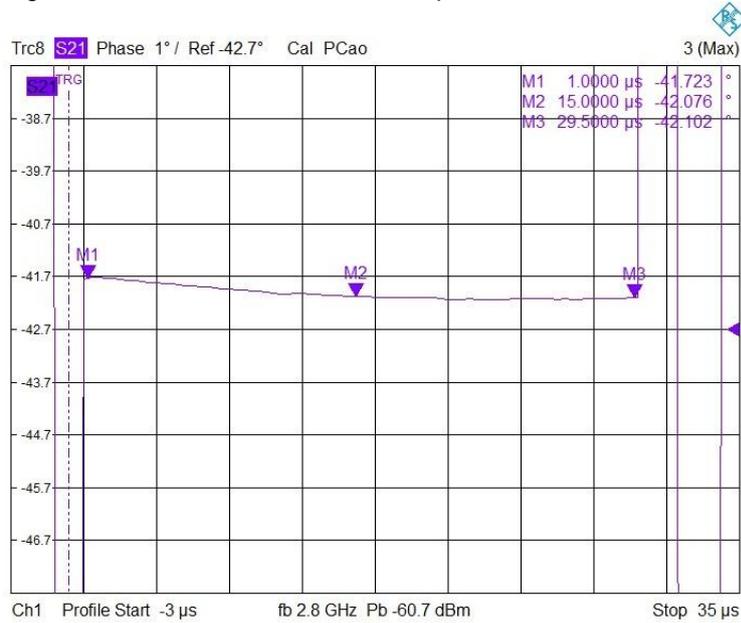


Figure 37: Test results of the pulse profile measurement. Phase measurement of S21 for total pulse width.

Figure 38 shows the behavior of S21 in terms of phase and magnitude.

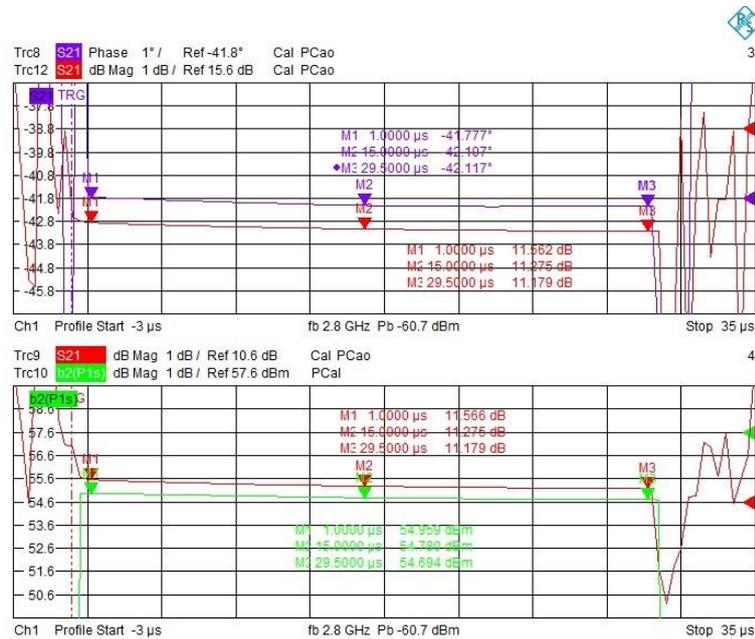


Figure 38: Test results of the pulse profile measurement. The magnitude and phase of S21, magnitude of wave quantities b2 total pulse width.

8 References

1. R&S ZVA Operating Manual, chapter Pulsed Measurements/Pulse profile Mode
http://www.rohde-schwarz.com/en/manual/r-s-zva-r-s-zvb-r-s-zvt-operating-manual-manuals-gb1_78701-29013.html
2. Thilo Bednorz, "A Network Analyzer System for Pulse Profile Measurements",
<http://ieeexplore.ieee.org/xpl/articleDetails.jsp?arnumber=5757070>
3. Thilo Bednorz, Roland Minihold, Kay-Uwe Sander, Frank-Werner Thümmler
Application Note 1MA124, "Tackling the Challenges of Pulsed Signal Measurements",
<http://www.rohde-schwarz.com/appnote/1MA124>

9 Ordering Information

Please note that a complete range of network analyzers, power amplifier, power sensor and power meter is available from Rohde & Schwarz.
For additional information about these instruments, see the Rohde & Schwarz website www.rohde-schwarz.com or contact your local representative.

Product Ordering Information		
Type of instrument	Designation and range	Order No.
Vector Network Analyzer		
R&S® ZVA 8*	Vector Network Analyzer, 300 KHz..8GHz, 4 Port	1145.1110.10
R&S® ZVA-K7	Pulsed Measurements	1164.1511.02
R&S® ZVA-K27	Pulse Generator	1164.1892.02
R&S® ZVA8-B16	Direct Generator/Receiver Access for the R&S® ZVA 8.	1164.0209.08
R&S®ZVA8-B21	Generator Step Attenuator Port 1	1164.0009.02
R&S®ZVA8-B22	Generator Step Attenuator Port 2	1164.0015.02
R&S®ZVA8-B23	Generator Step Attenuator Port 3	1164.0021.02
R&S®ZVA8-B24	Generator Step Attenuator Port 4	1164.0038.02
R&S®ZVA8-B31	Receiver Step Attenuator Port 1	1164.0044.02
R&S®ZVA8-B32	Receiver Step Attenuator Port 2	1164.0050.02
R&S®ZVA8-B33	Receiver Step Attenuator Port 3	1164.0067.02
R&S®ZVA8-B34	Receiver Step Attenuator Port 4	1164.0073.02
Extension Unit		
R&S® ZVAX24	Extension Unit, 10 MHz.. 24GHz	1311.2509.02
R&S® ZVA-B271	Pulse Modulator Source Port 1	1311.2573.02
R&S® ZVA-B272	Pulse Modulator Receiver Port 2	1311.2508.02
R&S® ZVA-B273	Pulse Modulator Source Port 3	1311.2596.02
Power Sensor and Power Meter		
R&S® NRP-Z211*	Two-Path Diode Sensor, 10MHz ... 18GHz, -60dBm... +20 dBm	1417.0409.02
R&S® NRP	Power Meter	1143.8500.02
R&S® NRP-Z4	USB Adapter(Passive)	1146.8001.02
Broadband Power Amplifier		
R&S® BBA150-D60*	Broadband Power Amplifier	5355.9004K40
Signal Generator		
R&S®SMF100A*	Microwave Signal Generator	1167.0000.02
R&S®SMF-K3	Narrow Pulse Modulation	1167.7804.02
R&S®SMF-K23	Pulse Generator	

* Other ZVA, Power Sensor, Power Meter and Amplifier models are available as well. More Options are available. The instrument's minimum configuration for this application is shown in the table. Please ask your local representative for a suitable configuration according to your needs.

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